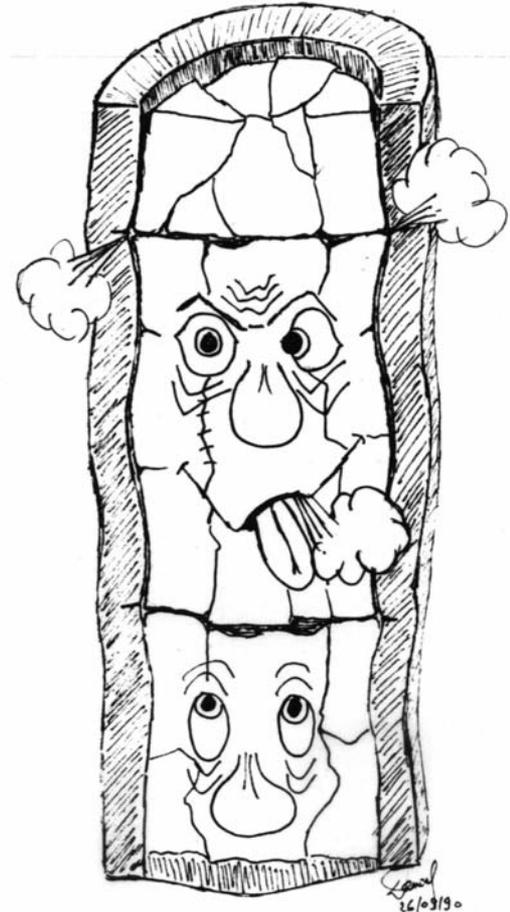


Nuclear fuels for the future

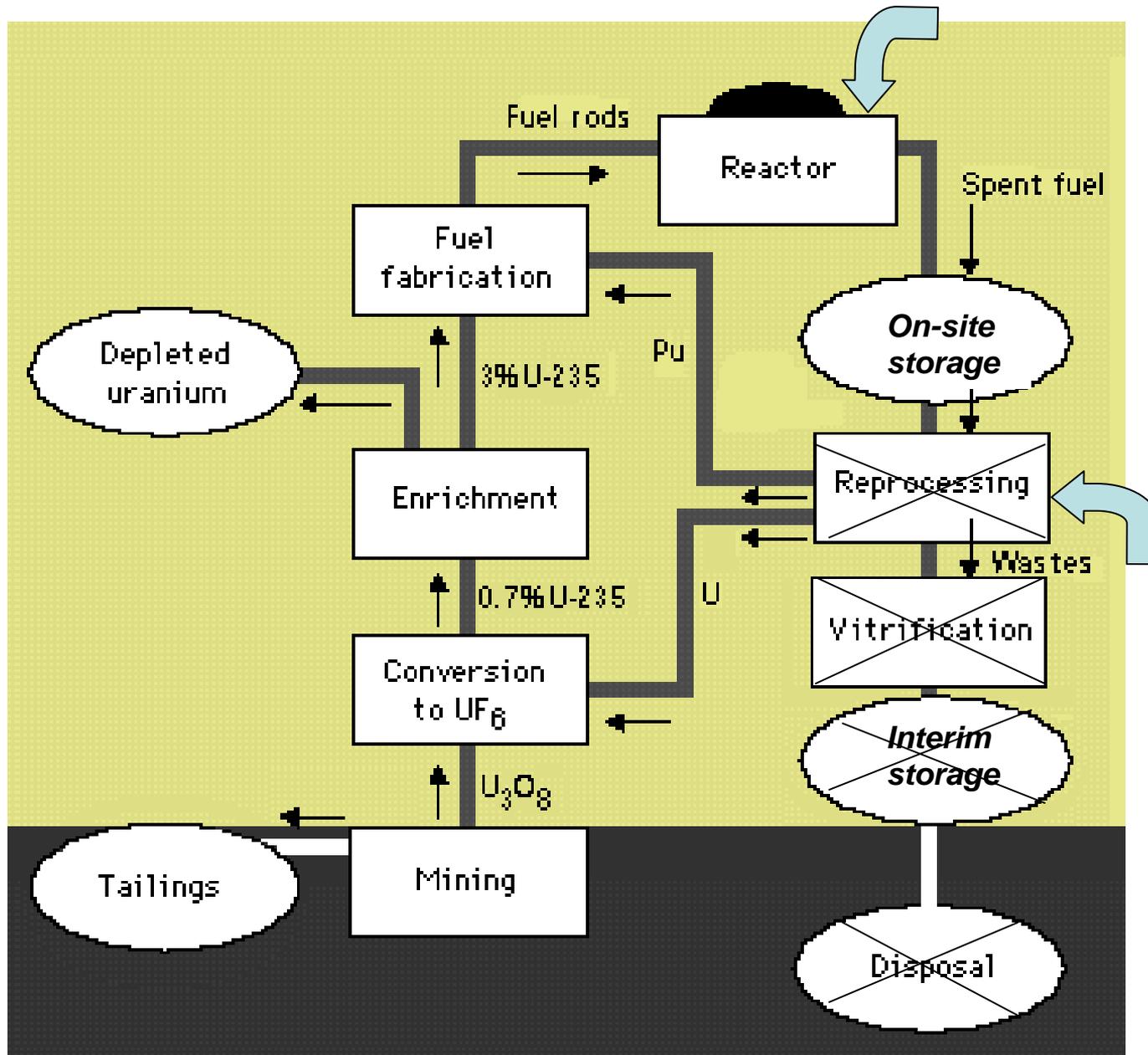
D. Olander

University of California, Berkeley

- 1. Core components and fuels of light-water reactors**
- 1. Fuel elements of LWRs**
- 2. Materials problems with oxide fuel**
- 3. Generation IV Reactor concepts**
- 4. New reprocessing schemes**



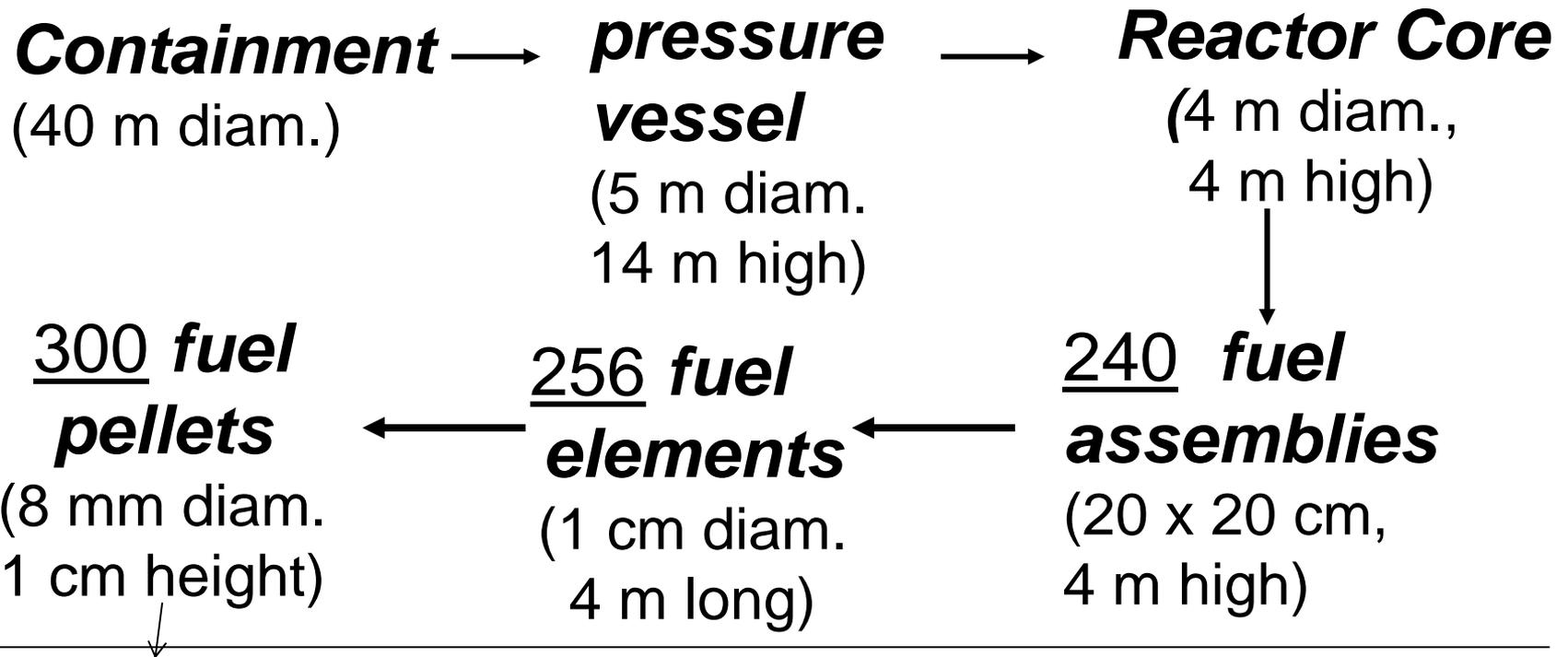
Standard Nuclear Fuel Cycle



Generations (“Gen”) of Nuclear Reactors

- Gen I – first nuclear electricity: **EBR-I, Shippingport, Magnox,**
- Gen II – Current fleet of *light-water reactors* (LWRs) - ***pressurized-water (PWR) or boiling-water (BWR); VVER; CANDU***
- Gen III - LWRs of completely new design – passive safety, fewer valves, shorter piping: **ABWR (GE-Toshiba), AP1000 (Westinghouse-AREVA)**
- Gen IV – completely new designs or resuscitation of old reactor types – **Sodium fast reactor; Very-high-temperature reactor**

1. Components of a 1000 MWe light-water reactor system (PWR & BWR)



Spent fuel load (U.S.)

$$18 \text{ M pellets} \frac{\text{core}}{\text{core}} \times 10 \text{ g} \frac{\text{pellet}}{\text{pellet}} \times \frac{1 \text{ core}}{6 \text{ yrs}} = 30 \frac{\text{tons}}{\text{yr-reactor}} \times 100 \text{ reactors} = 3000 \frac{\text{tons}}{\text{yr}}$$

2. Light-water reactor fuel element

Length ~ 4 m

Diameter ~ 1 cm

Cladding:

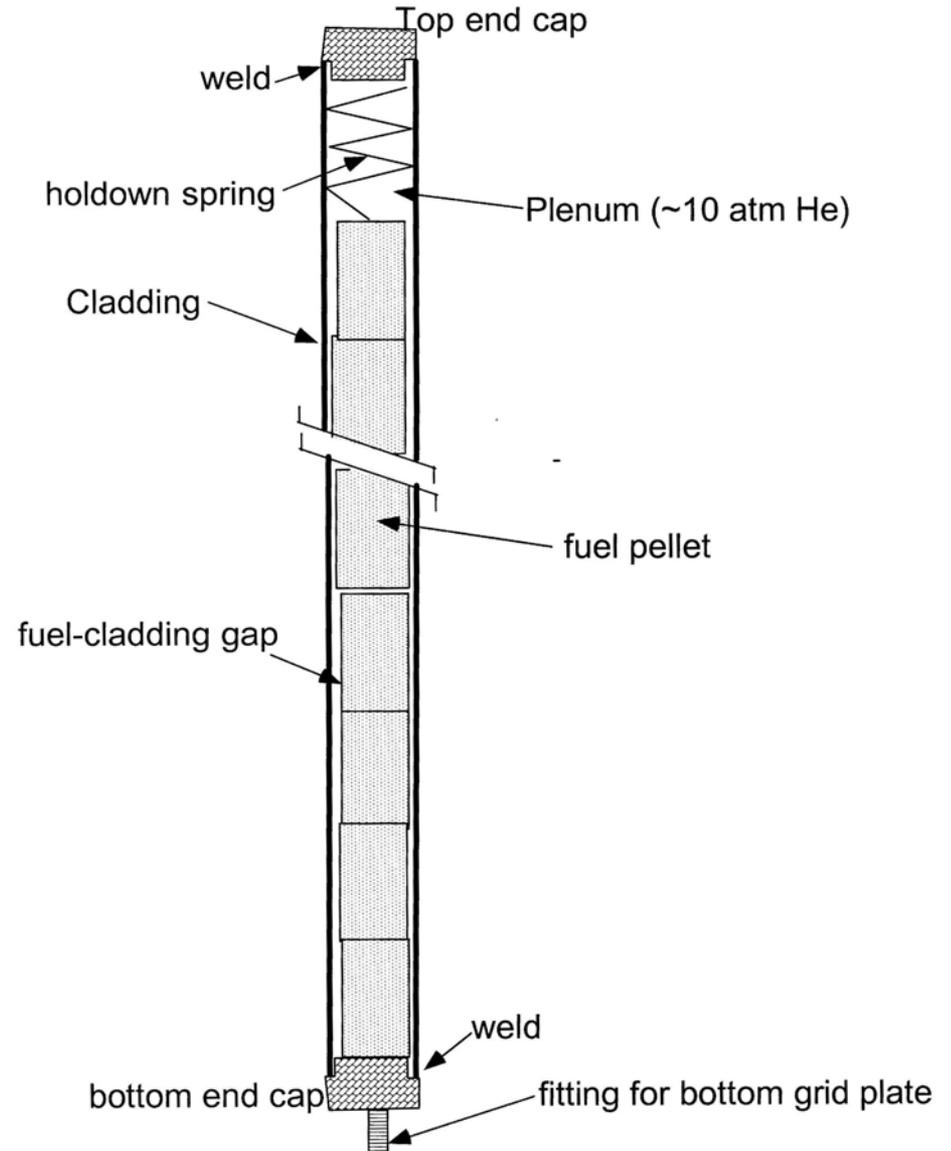
- Zr/1.5%Sn/0.5%FeCr
(Zircaloy)
- Zr/Nb (Zirlo, M5)

Fuel:

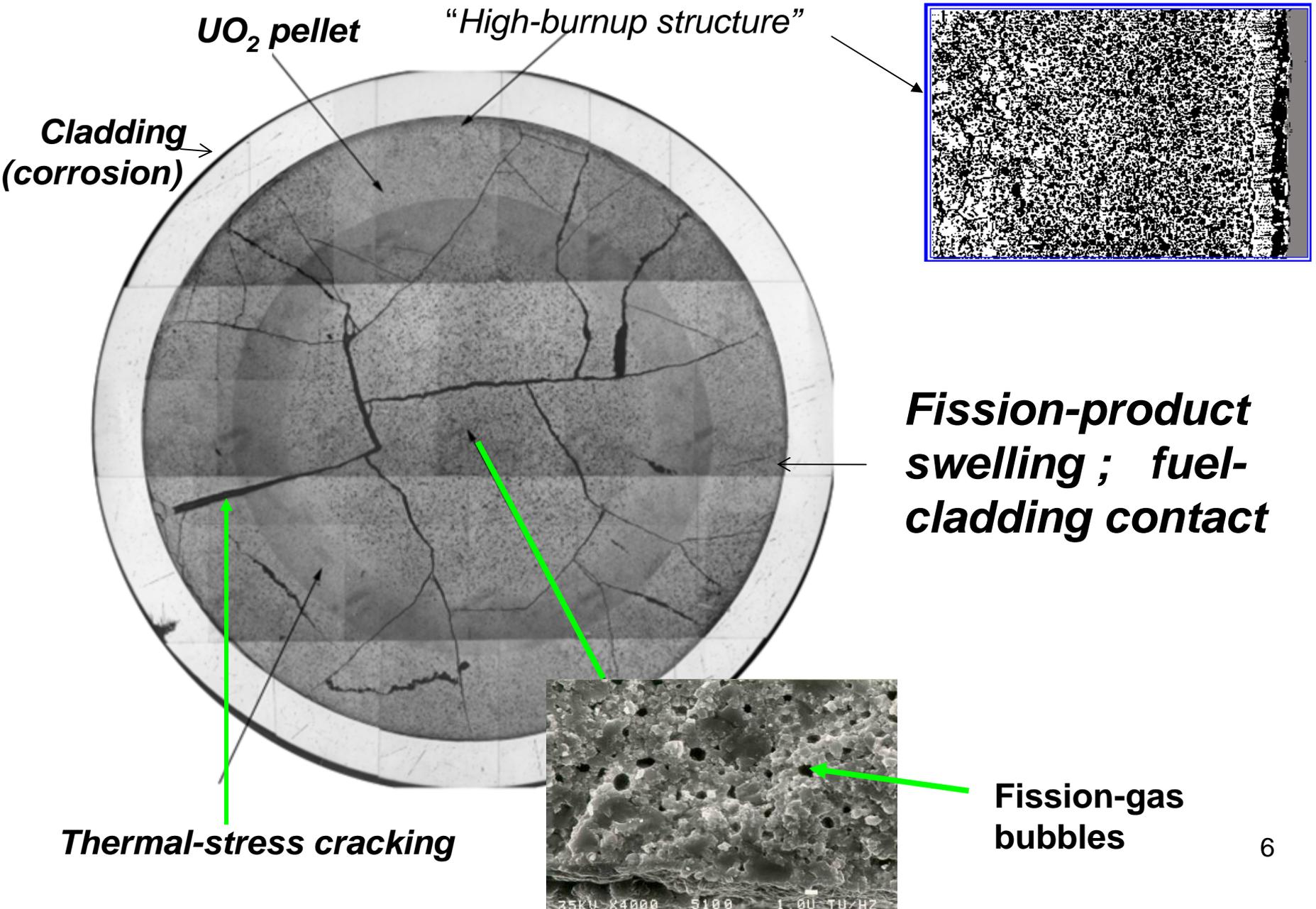
- UO_2 (oxide)
- $(\text{U,Pu})\text{O}_{2-x}$ (MOX)

Fuel-cladding gap (bond)

– helium at ~ 10 atm

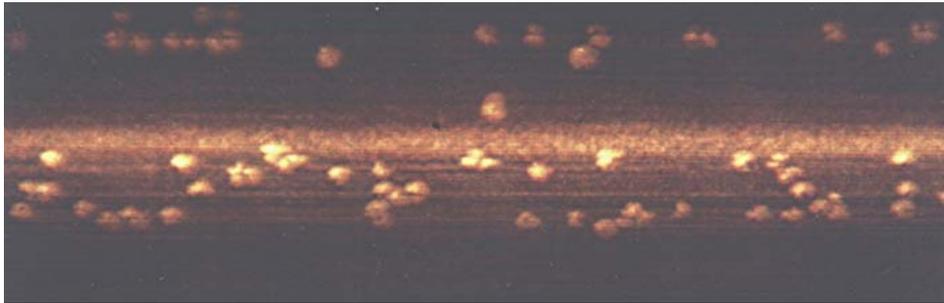


3. Problems with oxide fuel

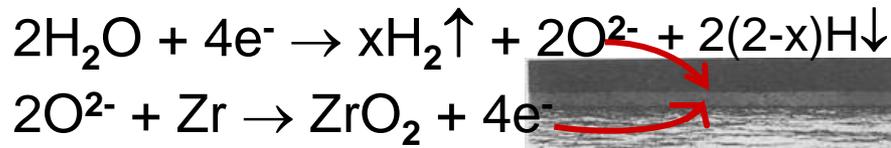
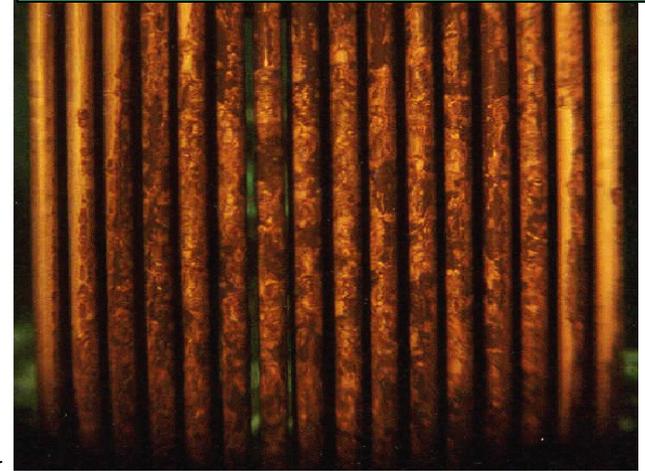


Cladding corrosion

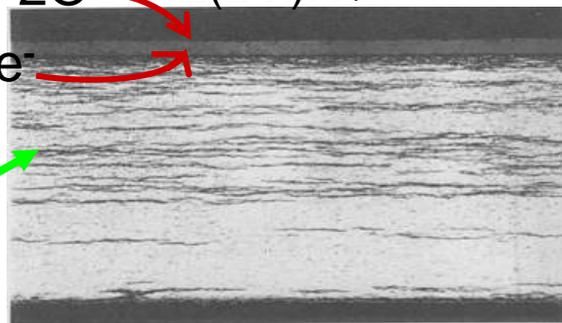
BWR - Nodular corrosion



PWR – uniform corrosion +



Hydride embrittlement



Oxide scale

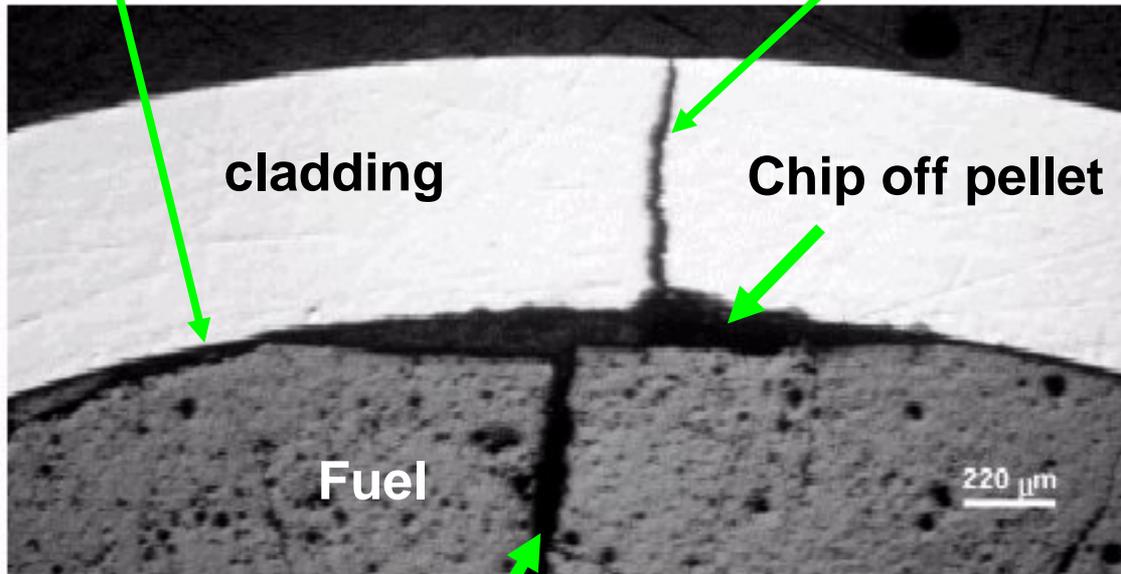
cladding

UO₂ pellet

Pellet-cladding interaction

Gap closes due to
fuel swelling

Stress-corrosion crack



Chip off pellet

Fuel

220 μm

Thermal-stress crack (fission-product path)

5. Generation IV reactor concepts

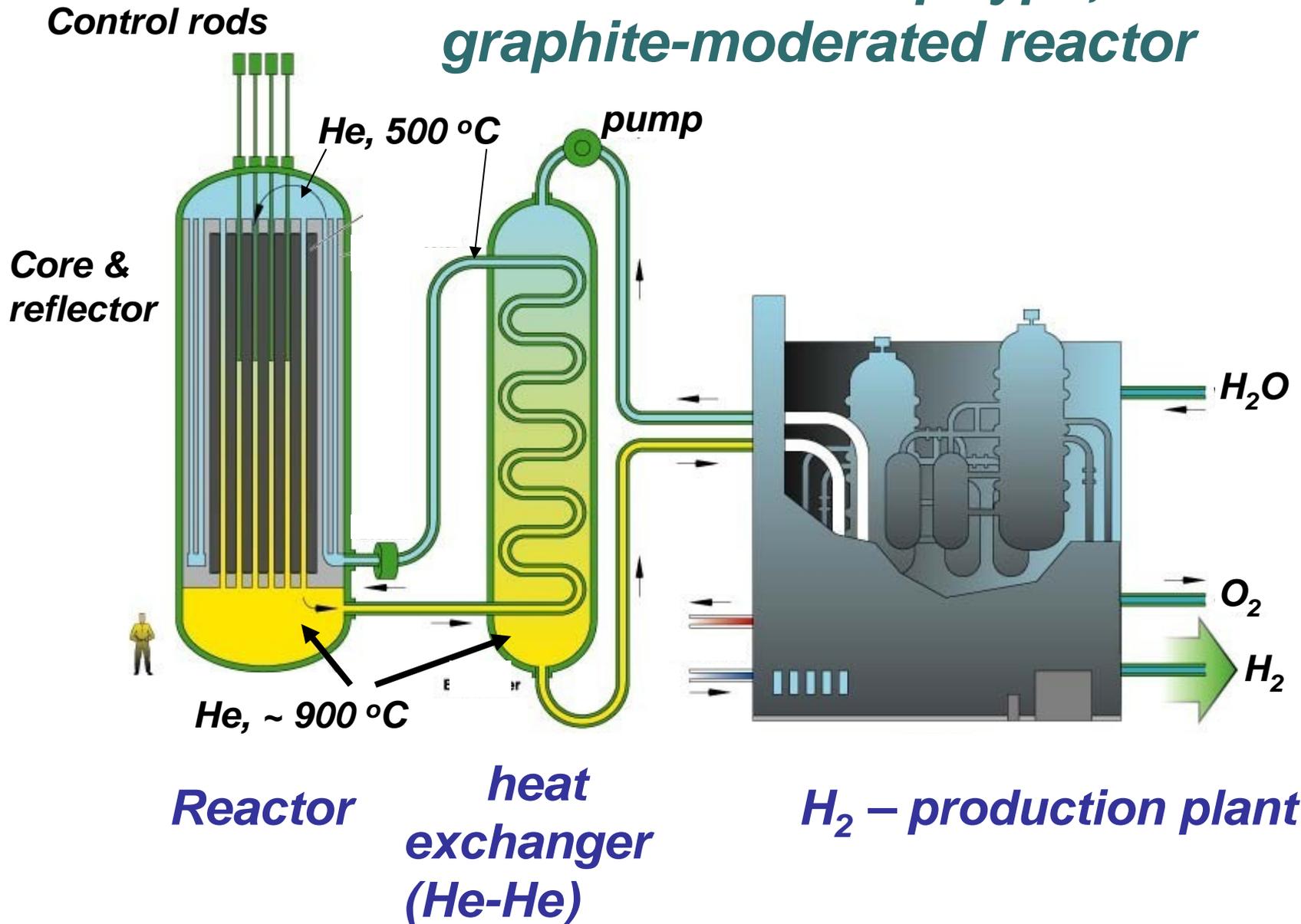
Reactor Coolant	Neutron energy	Purpose: electricity +:
Helium	Fast	H₂ production
Lead-bismuth	Fast	Encapsulated, 30-year life, small reactor ; BREST
Molten fluoride Salt	Thermal	Safety; H₂ production
→ Sodium*	Fast#	Burner of minor actinides from light-water reactors
Supercritical Water	Thermal	higher electrical efficiency than current LWRs
→ Helium*	Thermal&	Very-high temp. process heat (e.g. for H₂ production)

***current favorite**

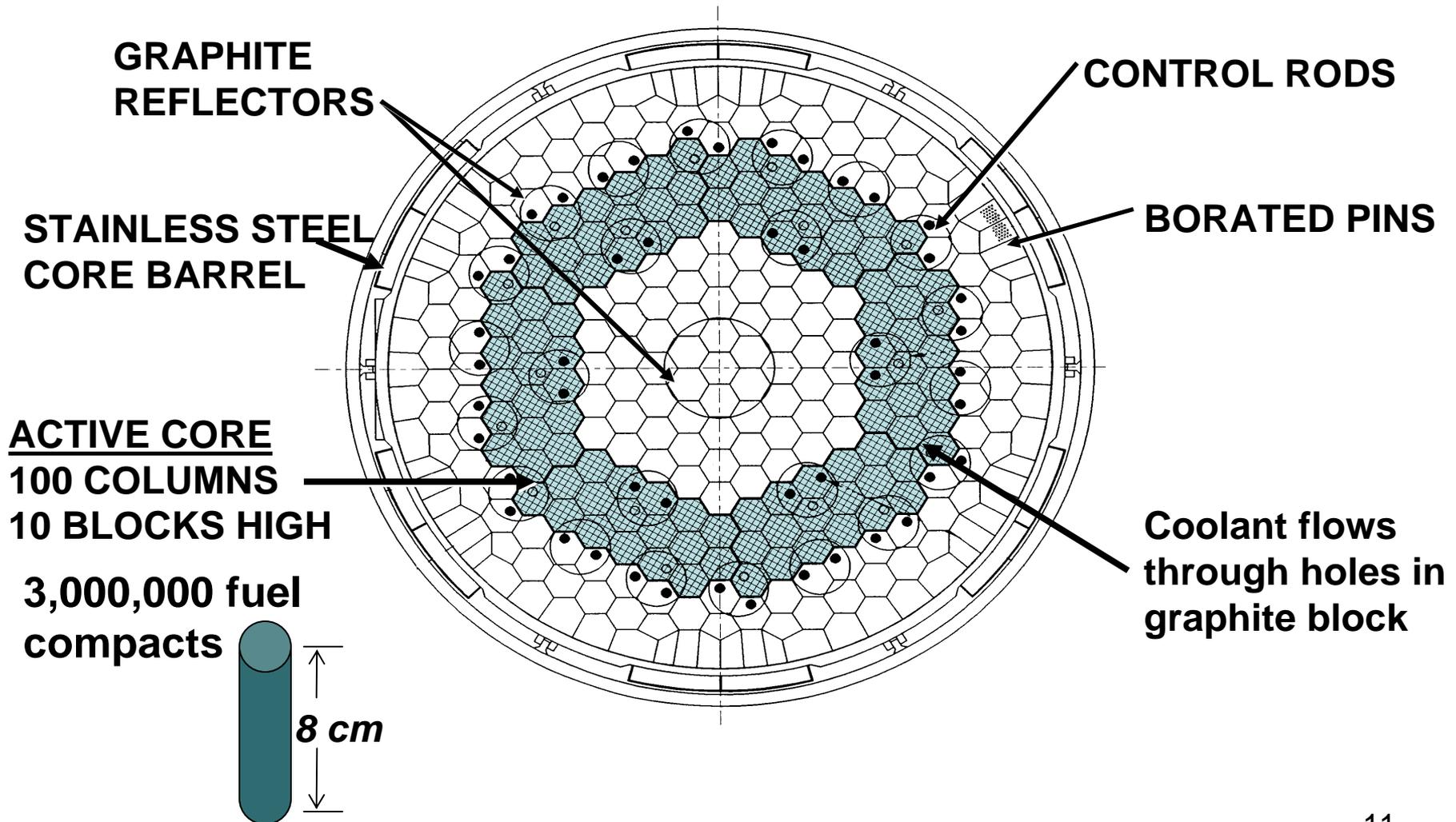
E_n ~ 1 MeV

& E_n ~ 0.025 eV

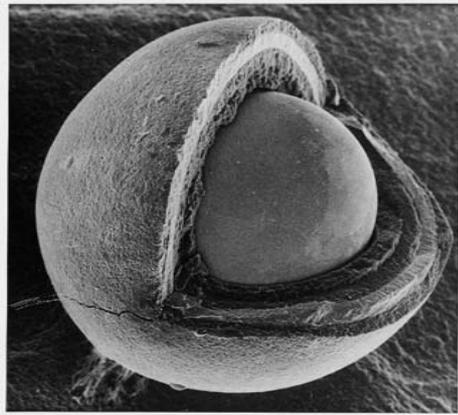
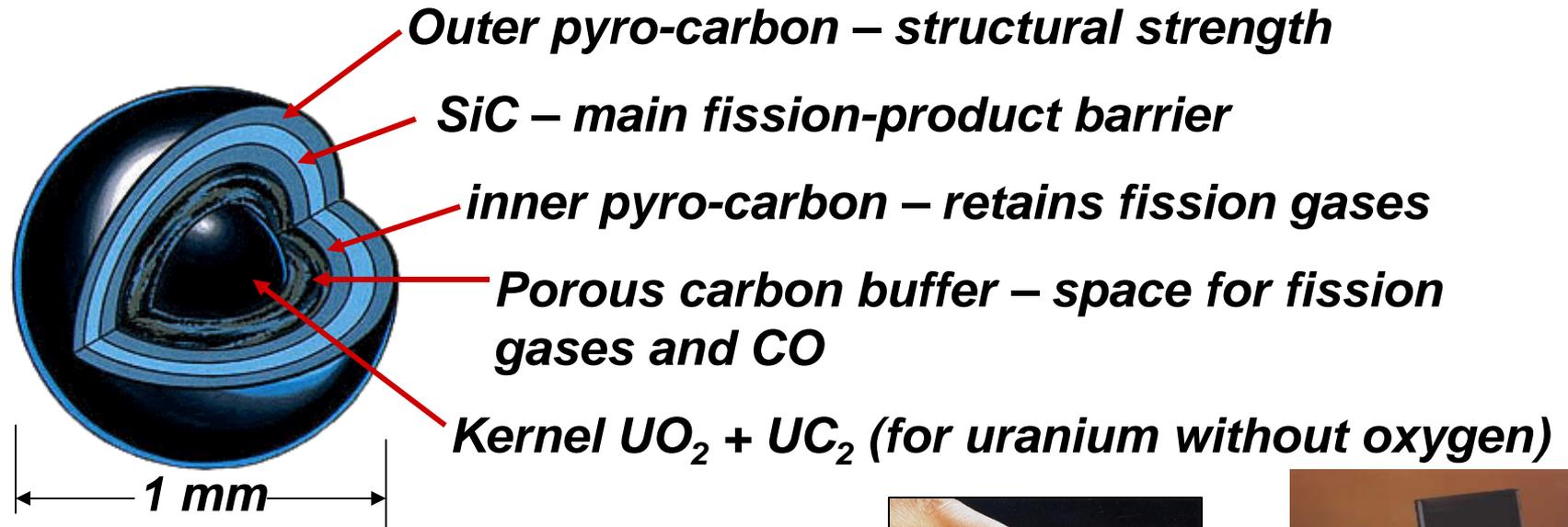
The VHTR – a loop-type, He-cooled, graphite-moderated reactor



Core configuration of the VHTR



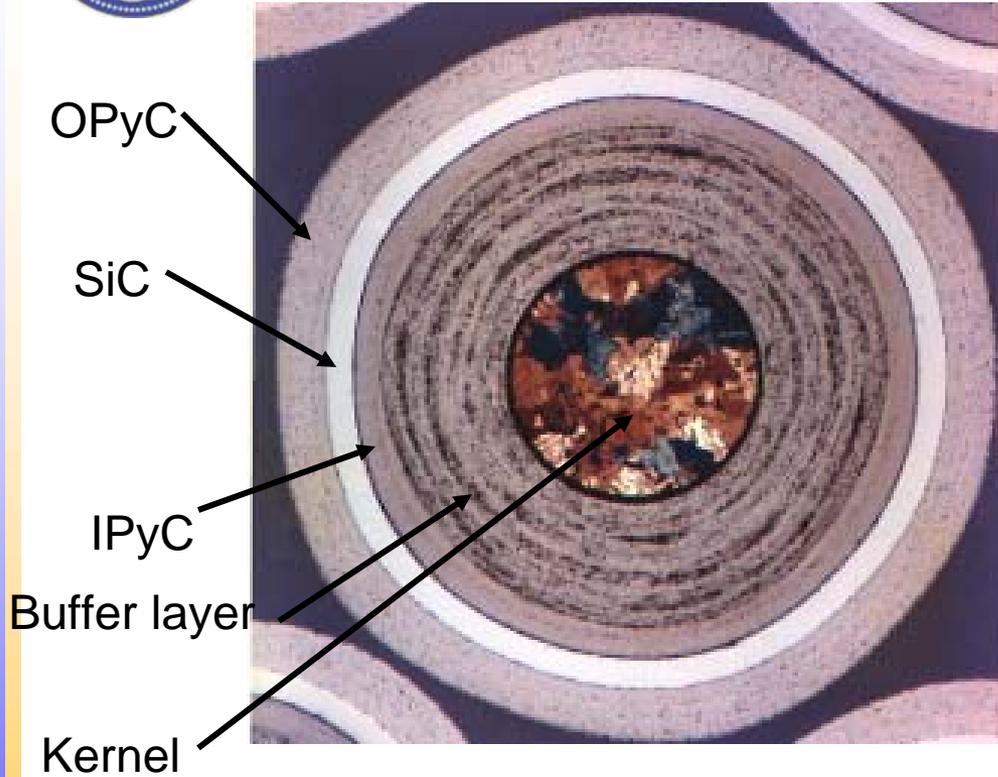
TRISO fuel for the VHTR



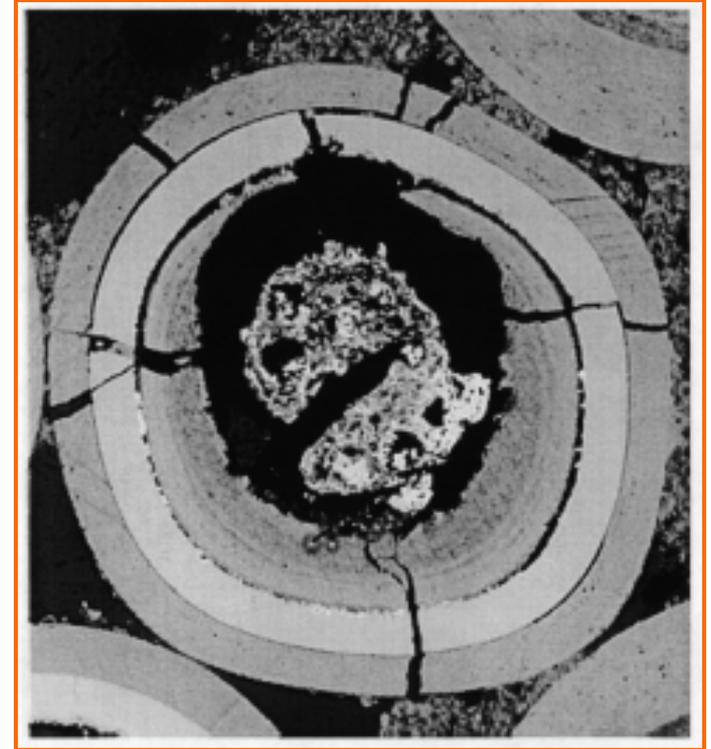
Final fuel forms



As-fabricated



Irradiated



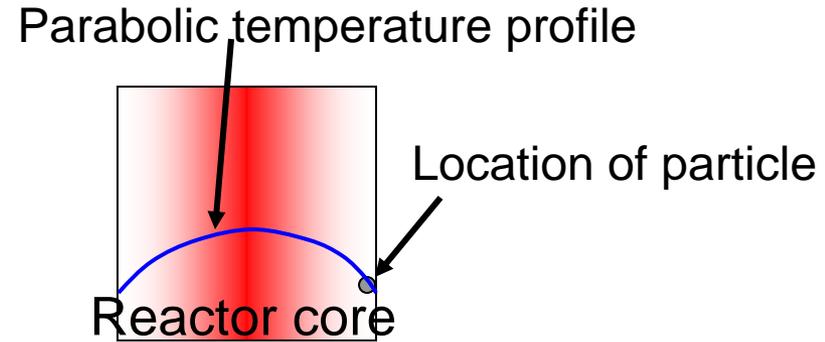
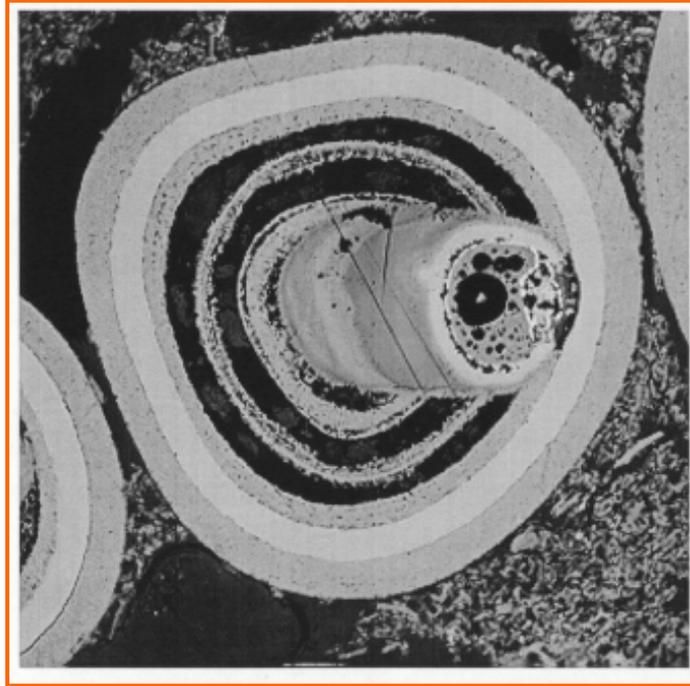
- Xe and Kr released from fuel kernel

- oxygen liberated from $(U,Pu)O_{2-x}$

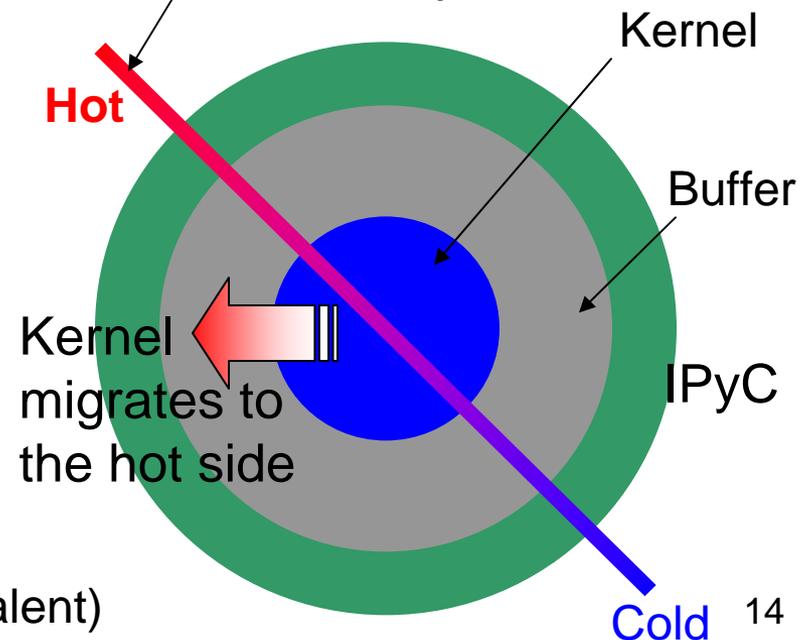
- $2C + O_2 \rightarrow 2CO$ reaction of carbon in buffer layer

Probably failed by overpressure due to fission gases and CO

Kernel Migration



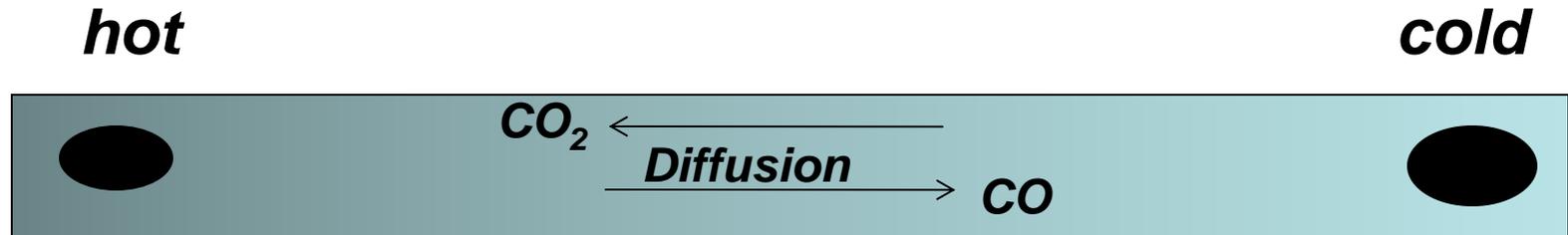
Temperature gradient across the fuel particle



CO produced from carbon in buffer and oxygen released from fuel: $2C + O_2 \rightarrow 2CO$

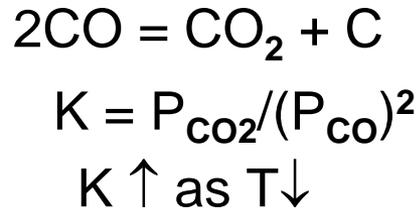
Why O released from fuel? U in UO_2 binds two O; fission products on average bind only ~ 1.67 O (most soluble fps are trivalent or divalent)

Mechanism



Low P_{CO_2}

small K
 CO_2 decomposes,
Produces CO and
consumes C



High P_{CO_2}

Large K
 CO decomposes,
Produces CO_2
and **produces C**

***\therefore kernel moves into space made by
gasification of C – i.e. to hot side***

Solution?

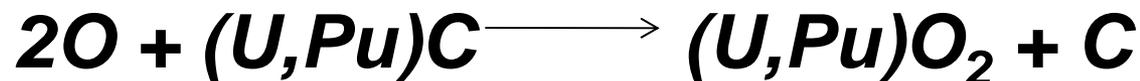
Add coat of ZrC around kernel



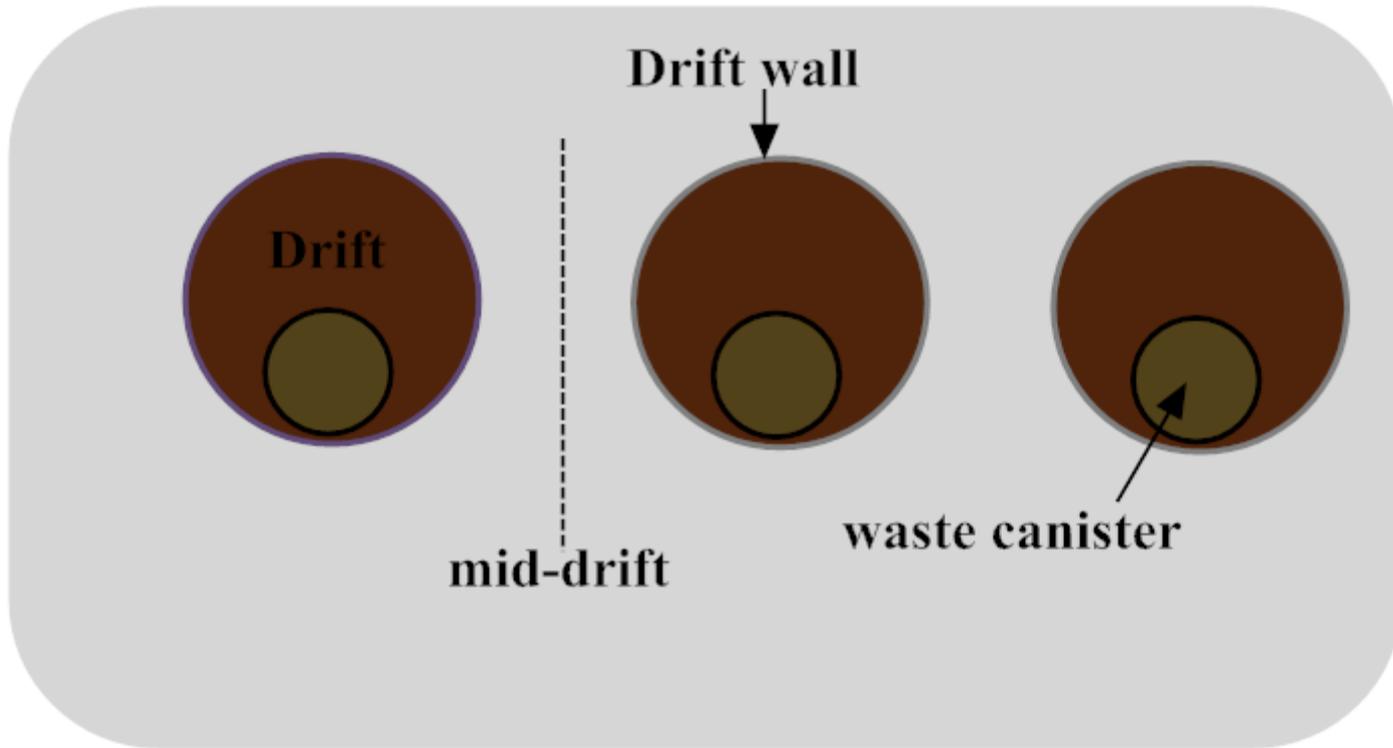
- ***K large, p_{O_2} reduced***
- ***If p_{O_2} decreased, p_{CO} is reduced***
- ***eliminates both the CO overpressure and kernel migration***

Use (U,Pu)O₂ + (U,Pu)C fuel in kernel

- ***Fission in carbide releases C, not O***
- ***O released from oxide consumed by (U,Pu)C***



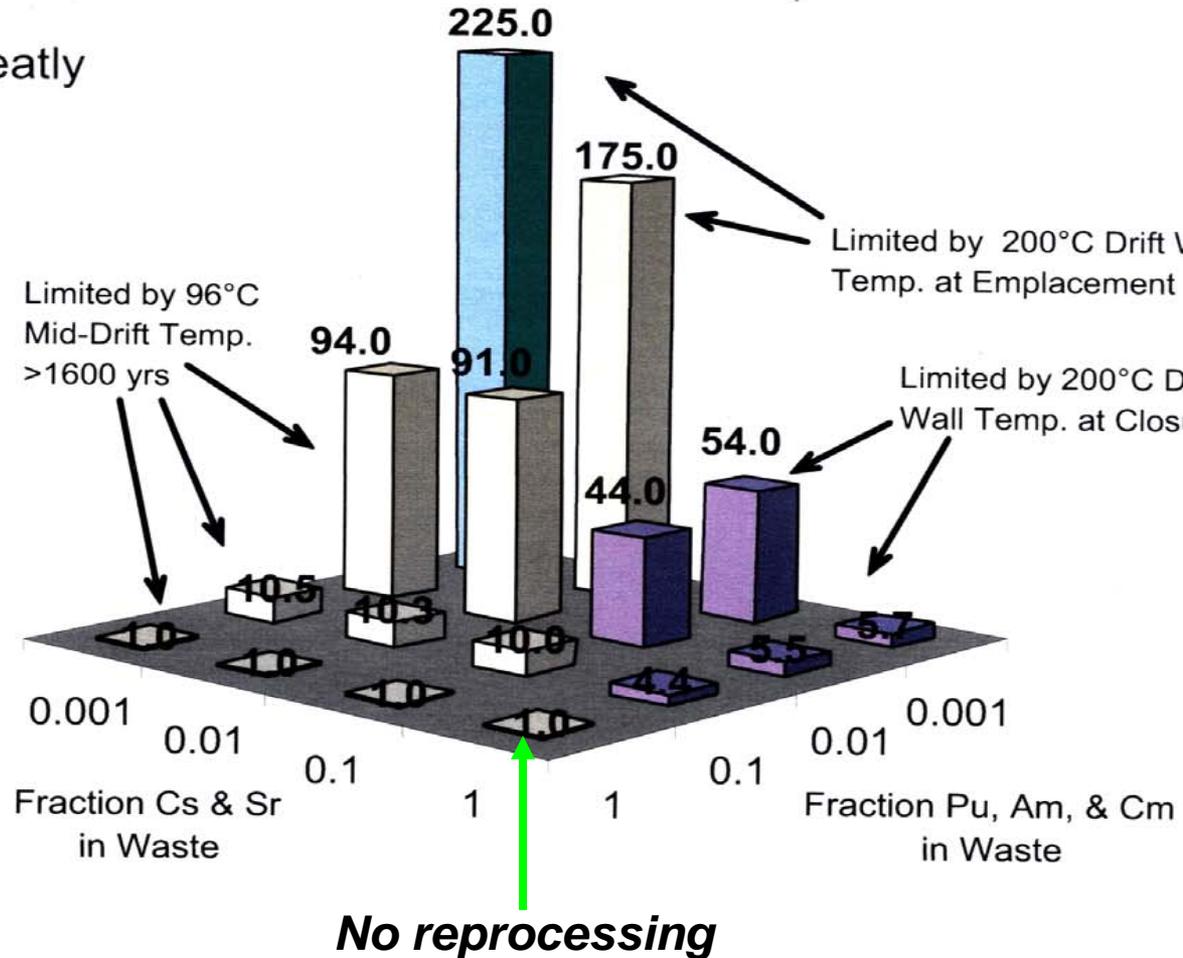
Geologic Repository



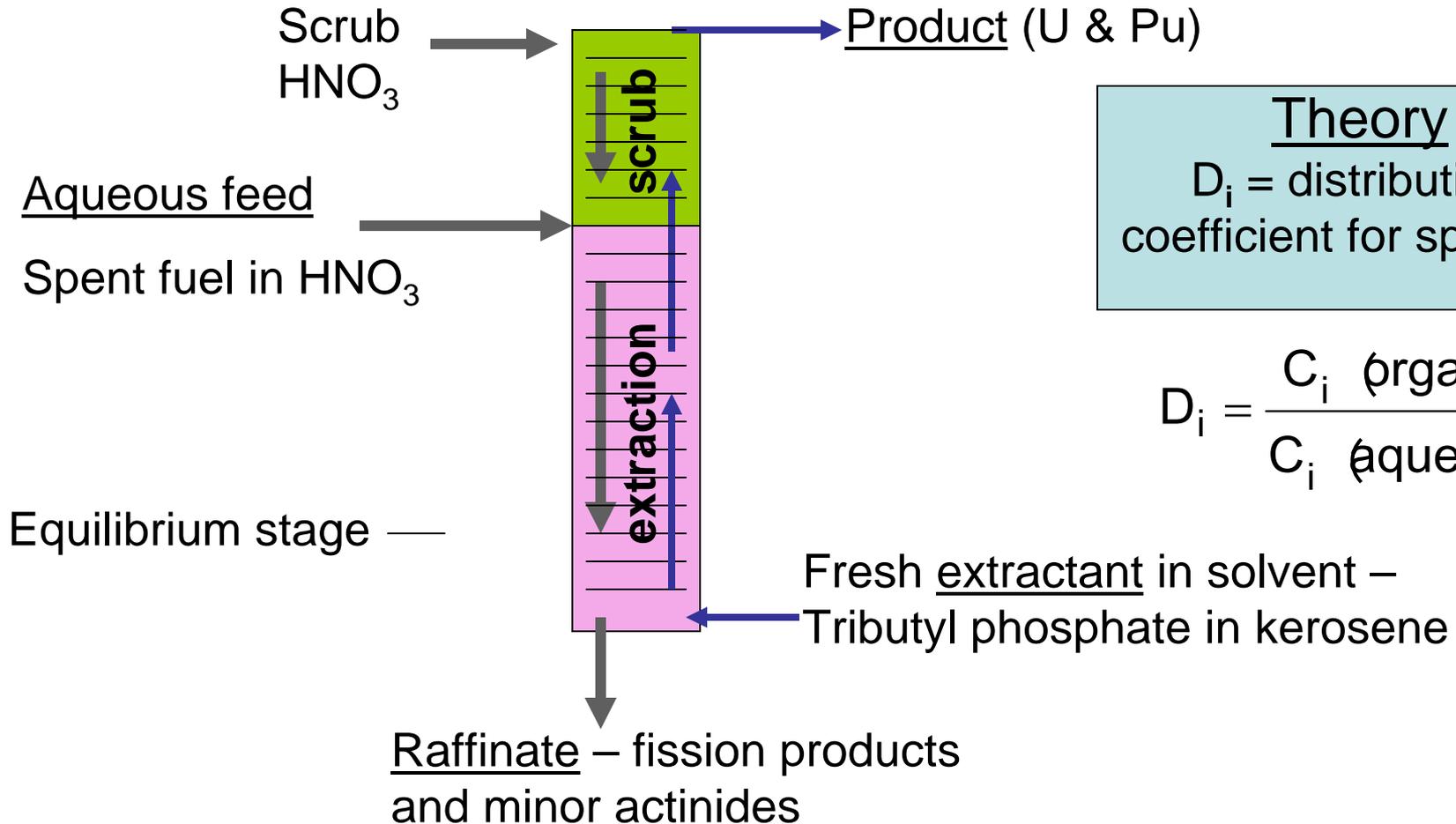
Why reprocessing is necessary

- Removal of Cs, Sr and TRU greatly reduces the heat load on the repository
- Assumptions:
 - Burnup = 50 GWd/MT
 - Separation in 25 years
 - Emplacement in 25 years
 - Closure in 100 years

Numbers on top of the columns represent the ratio of the quantity of reprocessed waste to the quantity of spent fuel that can be placed in a drift in repository



PUREX Solvent Extraction Process ~ 1950



New reprocessing requirements

- ***Pure Pu must not be separated***
- ***Cs & Sr must be separated from other fission products***
- ***Minor actinides to be separated (Np, Am, Cm)***
- ***Tc to be separated***

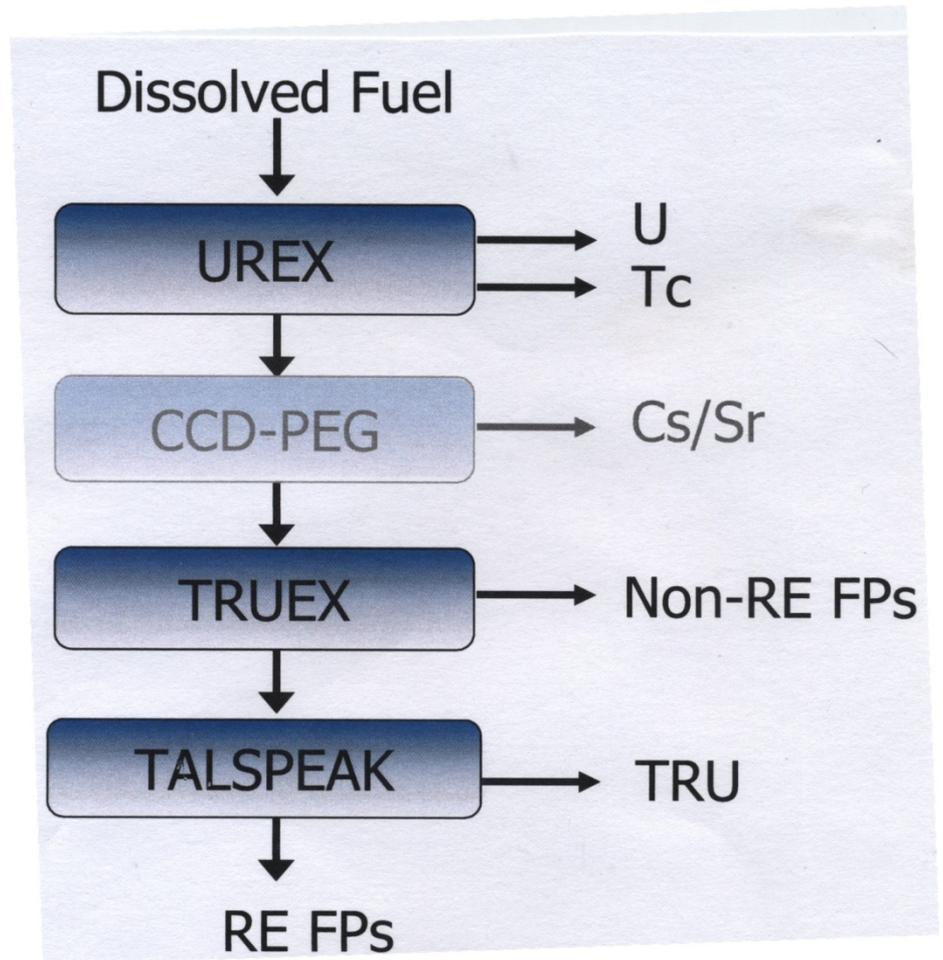
The UREX1a reprocessing suite

UREX = **UR**anium **EX**traction

CCD-PEG* = shorthand for extractant used

TRUEX = **TR**ans**U**ranium **EX**traction

TALSPEAK = **T**rivalent **A**ctinide/**L**anthanide **S**eparation by **P**hosphorus-reagent **E**xtraction by **A**queous **K**omplexes

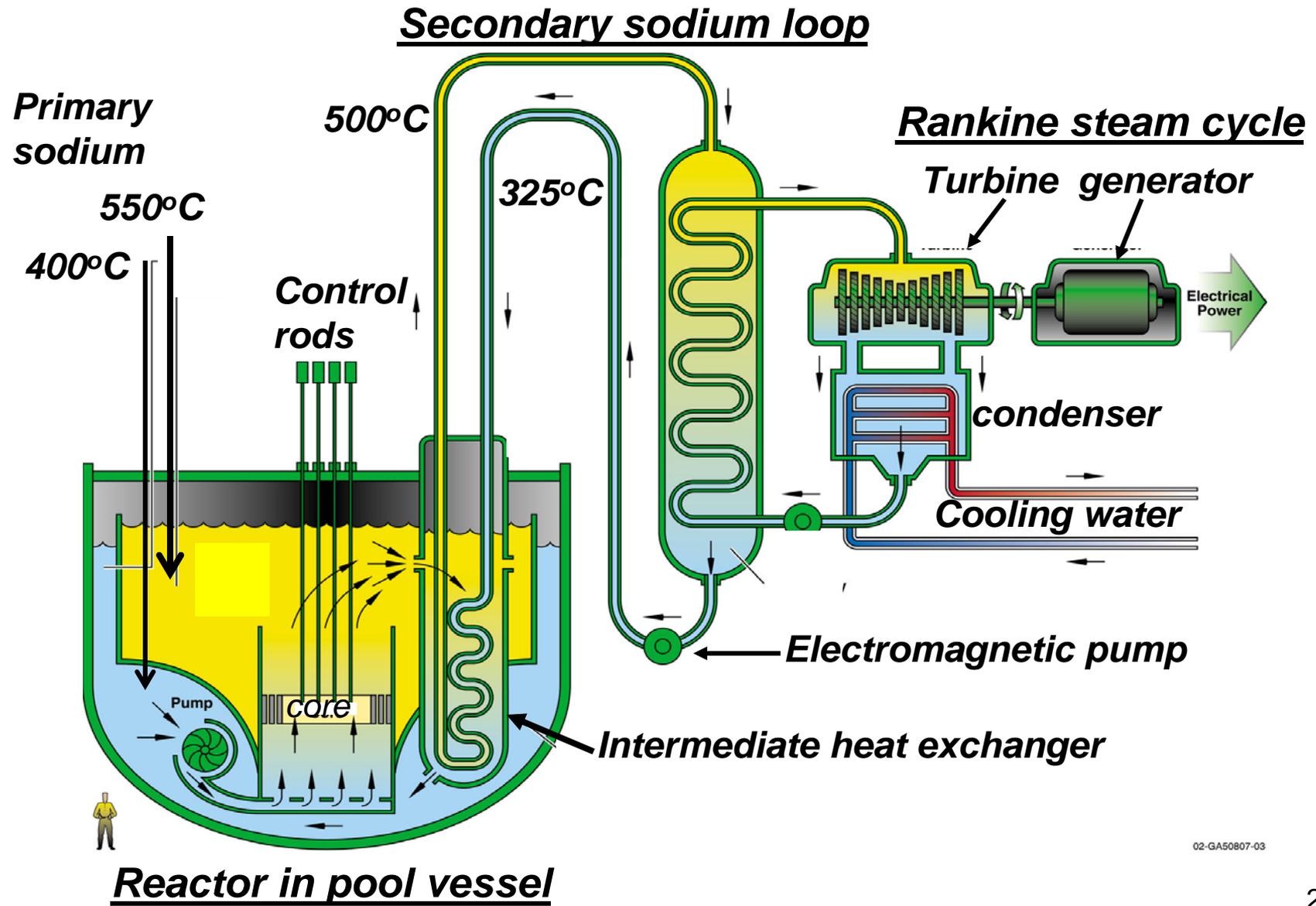


* Developed in Czech Republic, Russia

REMAINING PROBLEMS

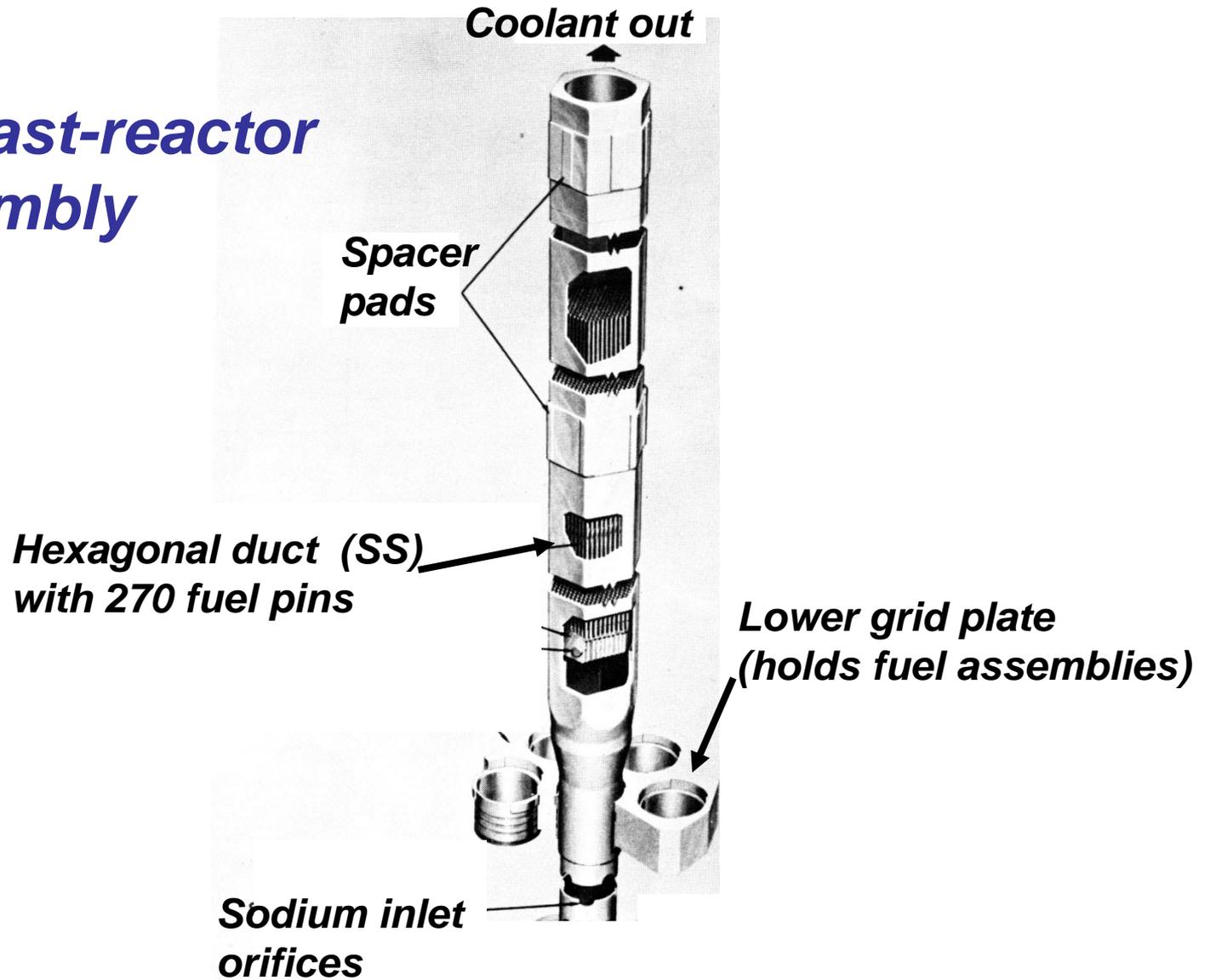
- Stability of exotic organic extractants in the high radiation field of the fission products
- Sensitivity of distribution coefficients to extraction conditions (pH, concentration of extractants, temp., oxygen potential)
- Inherent difficulty of some separations (esp. TRU from RE fp – both are trivalent)
- Conversion of products to solid wastefoms suitable for disposal in repository
- Lack of even pilot-plant experience with TRUEX and TALSPEAK

Sodium Fast Reactor (SFR)



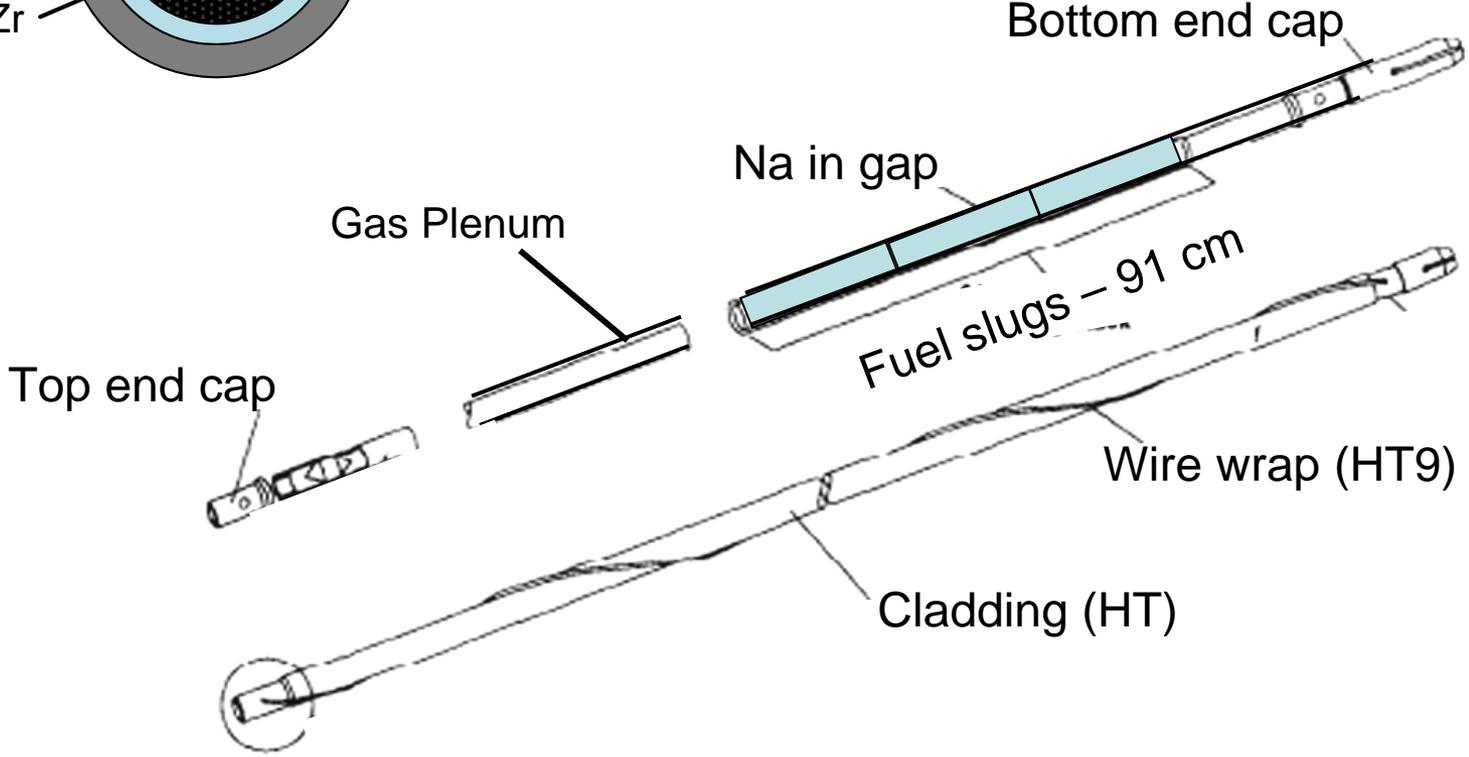
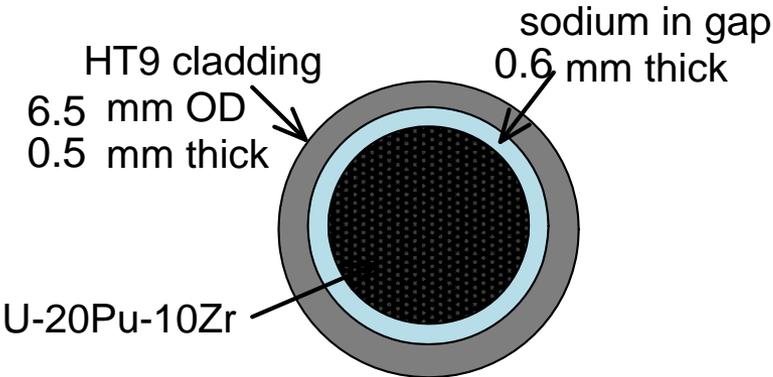
02-GA50807-03

Sodium fast-reactor fuel assembly



Metal fuel for SFR

U-20%Pu-10%Zr (+ MA)



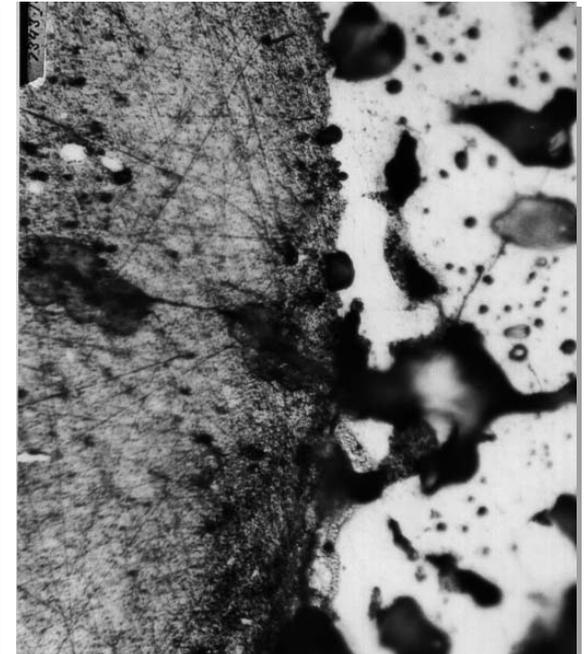
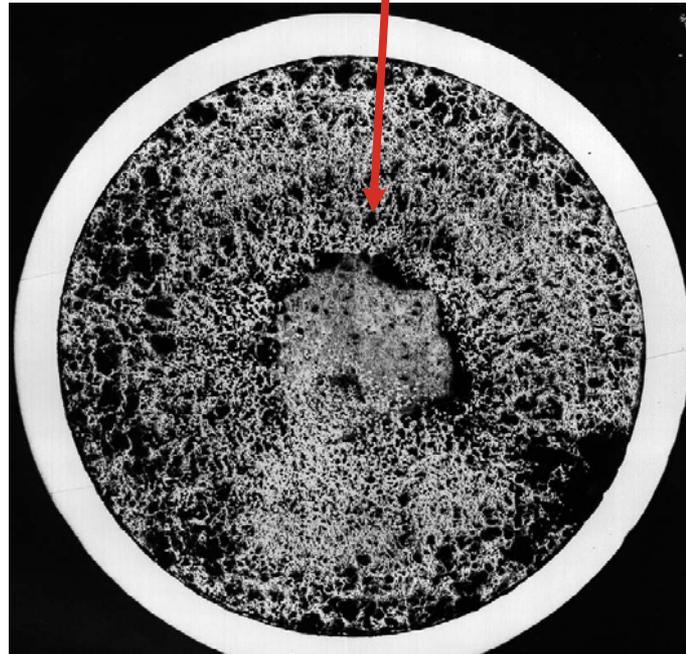
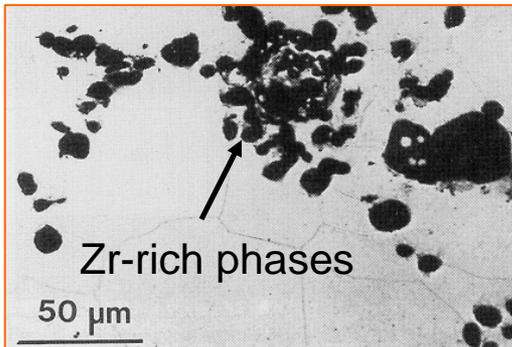
Metal Fuel Performance Phenomena

- Irradiation growth: ~ 3% at 14% burnup of metal atoms
- Fuel swelling and fuel-cladding mechanical interaction (FCMI)
- Gas release
- Fuel-cladding chemical interaction (FCCI)
- Fuel constituent redistribution

Low-Melting Phase

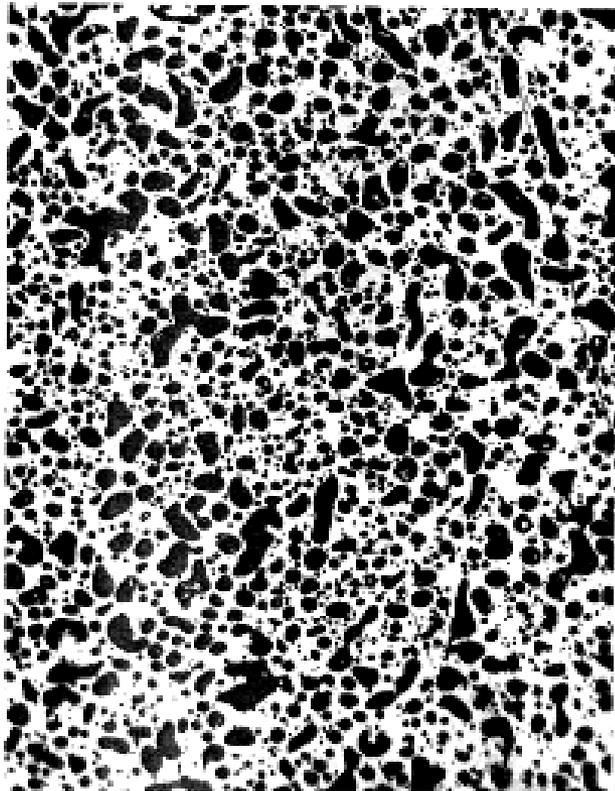
La, Ce, Pr, Nd, Pu react with SS cladding

as-fabricated



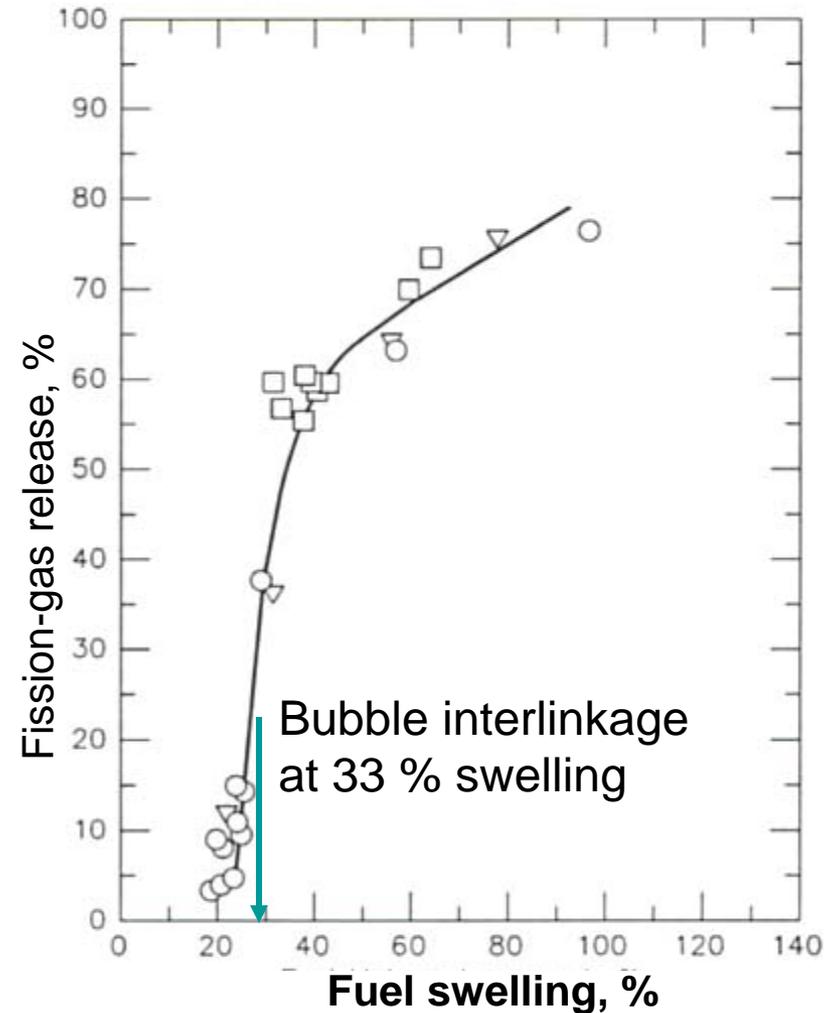
Swelling & Gas Release in metal fuel

Gas
bubbles



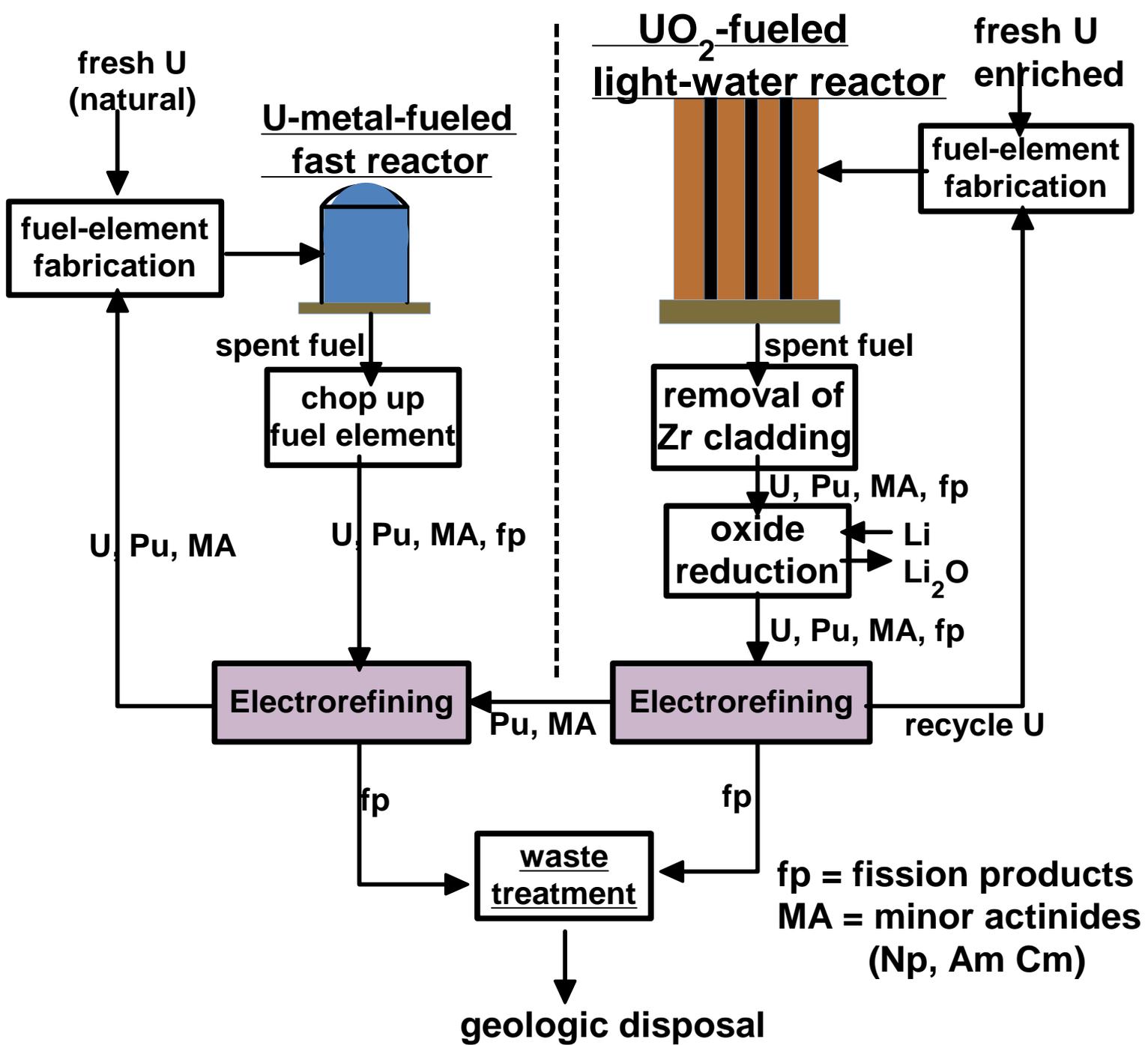
100 microns

2% FIMA (fissions per initial metal atom)

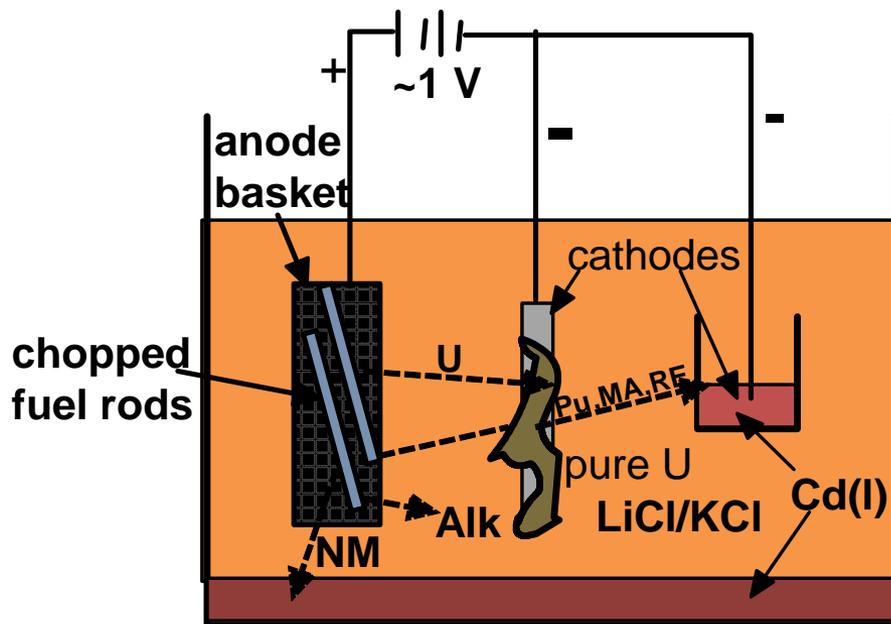


Pyroprocessing

- What is it? A high-temperature, nonaqueous electrochemical method of reprocessing spent nuclear fuel to separate the valuable constituents from the radioactive waste
- Motivations:
 - nonproliferation (plutonium)
 - recovery of uranium
 - sequestering of radioactive wastes
 - destruction of “minor actinides” (Np, Am, Cm) and Pu



Electrorefiner



- spent fuel dissolved/reacted in SS anode basket
- high-purity U transferred to SS cathode
- Pu and the minor actinides transferred to Cd(liq) cathode
- Cd puddle collects noble-metal fission products

fission products: NM = Rh, Ru, Pd; Alk = Na, Sr, Ba; RE = La,...Y

<u>Stable</u> (in salt phase)	<u>Electro-transportable</u>	<u>stable</u> (in Cd pool)
Cs, Ba, Sr	U, Pu, MA, RE	Mo, Pd, Rh, Ru

Electrotransport rate = $i/3\mathfrak{F}$; $i \propto V \times X_{M^{3+}}$

DOE's NGNP program

NGNP = Next Generation Nuclear Plant (Gen IV)

- ***six reactor types; two are favored:***

- VHTR: 5-layer fuel spheres; He cooled, graphite moderated. 900°C outlet temp. For power and/or H₂ production.

- Aqueous reprocessing of spent fuel

- SFR: metal fuel rods; sodium-cooled; unmoderated. For power and burning of minor-actinide elements from current fleet of LWRs.

- Pyrometallurgical reprocessing of spent fuel

- ***Neither are new designs***

- ***Demonstration plant circa 2020?***